

Production of KMnO_4 Modified Activated Carbon Fiber Filter from Pineapple Leaf Carbon Fiber for Fe^{3+} and Ca^{2+} Ions Adsorption

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Abstract

Objectives: The effects of ratios of KMnO_4 modified activated carbon fiber, zeolite, and sintering temperature for filter preparation were studied. The Fe^{3+} and Ca^{2+} ions removal by filter were also evaluated. **Methods/Statistical analysis:** The filters were characterized by XRD, FTIR, SEM-EDS, and BET analyzer. The percent drying shrinkage, percent firing shrinkage, percent total shrinkage, percent mass yield, density, and hardness were measured. The adsorption isotherms for Fe^{3+} and Ca^{2+} ions of the modified filter materials were also studied. **Findings:** The shrinkages and density properties increased with increasing sintering temperature and decreasing carbon fiber content, but hardness and mass yields showed a reverse trend. The filter has high content of MnO_2 , Si and Al oxides, P- and O-contain functional groups, montmorillonite, and kaolinite. The BET, pore volume and pore size of the sintered filter materials are quite lower than those of the starting materials due to the effects of the functional groups on the filter surface. **Application/Improvements:** Langmuir isotherm and Freundlich isotherm were fitted for both Fe^{3+} and Ca^{2+} adsorption by the modified filter with theoretical maximum adsorption capacity of 45.25 and 23.53 mg/g, respectively.

Keywords: Activated Carbon Fiber Filter, Adsorption Isotherm, Ca^{2+} , Fe^{3+} , KMnO_4 , Pineapple Leaf Carbon Fiber

1. Introduction

Various technologies for drinking water production are available with low cost and operating without electricity¹. Activated carbon is usually used for water purification. It is made from materials with high carbon content through carbonization and an activation process. A porous structure and its adsorption properties can be obtained in carbonaceous materials either via chemical or physical activation². Adsorption using activated carbon is strongly influenced by the surface area and surface charge³. Activated carbon fiber filters have also been used in a wide range of applications including air purification, dehumidification, and water purification, due to their large specific surface area, high adsorption capacity and rate, and specific surface reactivity⁴. Natural bio-fiber, as a starting material for activated carbon, can be produced from agricultural waste. Bio-fiber with low cost and high abundance can be extracted from pineapple leaf as reported^{5,6}. Pineapple leaf fiber exhibits high specific

strength and stiffness. It has a ribbon-like structure and consist of a vascular bundle system present in the form of bunches of fibrous cells, which are obtained after mechanical removal of all of the epidermal tissues⁷. It has many potential applications similar to other natural fibers such as plastic reinforcement, sound and thermal insulations⁸. For water filter production, activated carbon or activated carbon fiber can be mixed with clay minerals to form the final composite. Clay minerals are the most important inorganic components in soil due to their excellent mechanical and chemical properties⁹. Kaolinite ($\text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2 \cdot 2\text{H}_2\text{O}$) is the principal mineral in clay. It is a widely available, low cost, and high abundance material¹⁰. It consists of silica tetrahedron layers linked to alumina octahedron layers through hydrogen bonding between the tetrahedrons' basal oxygen and the hydroxyls from the octahedron layers³. The other clay mineral that has been widely used as filter is zeolite. Zeolites have a great capacity for cationic exchange and an affinity for heavy metals with high surface area and unique

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pore characteristics. They also have three-dimensional structures consisting of silica and alumina tetrahedrons with a great number of pores in the structure³. The general formula for a zeolite is $\text{M}_{2/n}\text{O} \cdot \text{Al}_2\text{O}_3 \cdot x\text{SiO}_2 \cdot y\text{H}_2\text{O}$ where M is any alkali or alkaline earth element, n is the valence charge on that element, x varies from 2 to 10 and y varies from 2 to 7. The Al_2O_3 and SiO_2 are structural cations because they form the tetrahedral framework with oxygen¹¹. Zeolites have a negative charge (generated by isomorphous substitution of Si^{4+} by Al^{3+}), which is counter balanced by native cations (Na^+ , K^+ , Ca^{2+} and Mg^{2+}) and water molecules in their pores and channels. Zeolites have been used for coal steam gas water treatment¹², for removal of heavy metals (As, Cd, Cr, Cs, Cu, Fe, Hg, Mn, Ni, Pb, Sr, W and Zn) and ionic species (ammonium, chloride, fluoride, nitrate, phosphate and sulphate) from industrial sludge's, acid mine drainage, and for treatment of wastewater from domestic and industrial sources. In addition, fly ash zeolites find their application as sorbent medium in permeable reactive barriers and contaminant barrier liners for immobilizing the contaminant plume in soil¹¹. Bentonite also has good sorbent properties for cationic pollutants such as high cation exchange capacity, reduction/elimination of bleeding, enhanced mechanical strength, optimal pore size and consequently higher adsorption efficiency, better stability and durability, reusability, larger surface area, and even comparatively lower cost for water treatment. Bentonite is one of the most widely used, abundant, and low-cost natural clay mineral¹³.

For drinking water treatment, oxidation agents such as chlorine, ozone, or permanganate have been used to oxidize macro molecular organic materials and to convert them into biodegradable low molecular weight compounds, which can be combined with coagulation/flocculation process¹⁴. KMnO_4 is widely used in drinking water treatment to strengthen and improve the removal of contaminants. It is supposed to react with organic matter in water, and some KMnO_4 should be reduced to products, such as MnO_2 or other hydrated oxides¹⁵. Manganese oxide (MnO_2), which has low cost and is environmentally friendly, has been used for doping with transition metals on internal surfaces of macroporous carbon for super capacitors and oxygen reduction reaction electro catalysts¹⁶.

The natural water, groundwater, and wastewater from industries and communities have a high content of Fe

and Ca. Fe is found in groundwater in its most soluble form, Fe^{2+} ions, and in the oxide form, Fe_2O_3 ¹⁷. Iron is also present in high concentration in waste effluents from steel tempering, coal coking, and mining industries. Iron can have a detrimental influence on the taste of water. Fe^{3+} ions in human blood are toxic to tissues and organs¹⁸. In severe iron poisoning, much of the damage to the gastrointestinal tract and liver may be the result of highly localized iron concentration and free radical production leading to hepatotoxicity through lipid peroxidation and the destruction of the hepatic mitochondria. As a result of the iron storage disease caused due to iron poisoning develops and the liver becomes cirrhotic. Hepatoma, the primary cancer of the liver, has become the most common cause of death among patients with hemochromatosis. This is an iron storage disease that results from the inability of the intestine to keep out unnecessary iron. Instead, iron gets accumulated in the liver causing siderosis¹⁹. Iron in drinking water and water supplies causes many problems, such as reddish color, bad odor, metallic turbidity, and staining of laundry. Iron removal is among the most problematic issues for making of potable water. Its main issues involve taste, visual effects, and clogging. The presence of dissolved iron influences the taste and aesthetic quality of water. Depending on the type and amount of iron, people may notice a metallic taste and red discoloration. Furthermore, residual iron at levels above 0.3 mg/dm^3 may stain surfaces and clothes¹.

There are several methods for removal of iron from drinking water like ion exchange and water softening, activated carbon and other filtration materials, supercritical fluid extraction, bioremediation and limestone treatment, oxidation by aeration, chlorination, ozonation followed by filtration, by ash, by aerated granular filter, by adsorption, and by manganese greensand (through oxidation and filtration)¹. Soluble iron is also oxidized and precipitated by contact with higher oxides of manganese on the greensand granules. Precipitates are then filtered and removed by backwashing¹. Water softener removes Fe, which is in the dissolved form. Softening also removes calcium and magnesium ions, which are the primary minerals responsible for hard water. The treatment process consists of passing the water through an ion exchange resin bed. The Fe ions as well as calcium and magnesium ions in the water are exchanged for sodium (Na^+) ions, which have been temporarily stored in the resin material. As the hardness and Fe are removed from

the water, sodium is added proportionally¹. The most effective processes for the removal of these contaminants seem to be the use of activated carbons as highly porous materials as they have an extremely high surface area for contaminant adsorption¹. Ceramic-packed biotrickling filter, which contains an immobilized activated sludge, has also been set up for water purification²⁰. The double imprinted sorbent with chelating diamines²¹, nano-hydroxyapatite chitin/chitosan hybrid biocomposites¹⁹ were also used for Fe^{3+} ion adsorption.

In this work, activated carbon fiber filter from pineapple leaf fiber carbon doped with KMnO_4 was prepared. Activated carbon fiber filter was formed by mixing the plant material with clay, zeolite, bentonite, and borax (as fluxing agent). The effects of KMnO_4 and sintering temperature were studied. The filter products were characterized by XRD, FTIR, SEM-EDS, and BET analyzer. The Fe^{3+} and Ca^{2+} ion removal by the filter was studied as well.

2. Materials and Methods

2.1 Activated Carbon Fiber Preparation

Pineapple leaf fiber was collected after a mechanical milling process. Fresh pineapple leaves, which contain approximately 85% water, were cut to a length of 5 mm and milled with a disc mill. The milled materials were cleaned with water and air dried at room temperature for 3 days. The resulting dried crumb was ground with a high-speed grinder consisting of a stainless steel bowl and a rotating blade. The ground leaf is composed of fibrous

and non-fibrous materials. After that, pineapple leaf fiber was oven (SL 1375 SHEL LAB 1350 FX, USA) dried at 105 °C for 6 hours. Sieving the material with steel wire sieve (mesh number 60) separated the fibrous and non-fibrous materials. The dried pineapple fibrous material contains approximately 71% of cellulose, 20% of hemicelluloses, and 2% of lignin by weight⁵.

The dried pineapple leaf fiber was then carbonized at 500°C in an electric furnace (Fisher Scientific Isotemp® Muffle Furnace). The temperature was initially increased at a rate of 10°C/min and then kept constant for 1 h. The pineapple leaf carbon fiber was impregnated with 85% phosphoric acid using a weight/volume ratio of 1:1. The impregnated mixtures were oven dried at 105°C for 1 day and then activated at 500°C under partial oxygen of atmosphere. The temperature was also increased with a rate of 10°C/min up to 500°C and kept constant for 1 h. After that, the activated carbon fiber was modified with 5%wt of KMnO_4 and oven dried at 105°C for 1 day.

2.2 Filter Preparation

Zeolite (commercial grade), bentonite (commercial grade), and local clay (obtained from Tambol Tapoh, Muang District, Phitsanulok Province, Thailand), were ground and sieved (Laboratory test sieve, Retsch, Germany) to 200 mesh. These materials were mixed together with KMnO_4 modified activated pineapple leaf fiber carbon (40, 50, or 60wt %) to prepare mixtures containing zeolite (10, 20, or 30wt %), bentonite (10wt %), clay (10wt %), and borax ($\text{Na}_2\text{B}_4\text{O}_7 \cdot 10\text{H}_2\text{O}$) as the fluxing agent (10%wt) Table 1. The mixtures of all starting materials were wetted with



Figure 1. Samples of the rod form of the filters before sintering (a) and after sintering at 500°C (b), 600°C (c), and (d) 700°C.

Table 1. The ratios of raw starting materials in filter mixtures

No. samples	Ratios of raw materials in mixtures of filter (%wt)				
	KMnO_4 modified activated carbon fiber	Zeolite	Bentonite	Local clay	Borax
1	60	10	10	10	10
2	50	20	10	10	10
3	40	30	10	10	10

water (20% by volume) and then pressed into a PVC pipe ($\phi = 12.7$ mm, long = 50 mm) as shown in Figure 1(a). The wetted samples were dried in an oven for 24 h. The dried samples were then placed into a ceramic box and covered with foil, quartz powder, and closed by a lid. These samples were then sintered in an electric furnace under a reducing atmosphere at temperatures of 500°C, 600°C, or 700°C with 1 h soaking time. The percent of drying shrinkage and percent of firing shrinkage of the samples were measured by the methods of de in^{22,23} respectively. The percent mass yields of the sintered filters were also measured. The sintered samples were characterized by X-ray powder diffractometer (XRD, PW 3040/60, X' Pert Pro MPD) with a Cu tube anode, a Fourier transform infrared spectrometer (Spectrum GX, Perkin Elmer), scanning electron microscope equipped with energy dispersive spectrometer (SEM-EDS, LEO 1455 VP), and BET analyzer (Micromeritics TriStar II).

2.3 Fe Adsorption Experiments

The 1000 mg/dm^3 Fe^{3+} stock solution was prepared from 0.4827 g of iron(III) chloride hexahydrate (Merck, Germany) dissolved in deionized water, acidified with 1 cm^3 of 1 M HCl added, and diluted to 100 cm^3 with deionized water. Further solutions (3, 5, 7 and 10 mg/dm^3) were prepared from the stock solution by successive dilution.

Batch Fe^{3+} adsorption experiments were performed using the method of²⁴. The filters (0.1 g) were added to 50 cm^3 of Fe^{3+} solutions (3, 5, 7, 10 mg/dm^3) in a conical flasks and shaken continuously at 120 rpm at a temperature of 32 ± 2 °C. Following the adsorption, the aqueous phases were separated by centrifugation at 4000 rpm for 10 min and the final concentrations of Fe^{3+} ion in the solutions were determined by FAAS (Varian SpectrAA 220, Australia) with air-acetylene and cathode on Fe-hollow cathode lamp at 248.3 nm.

The amounts of adsorbed Fe^{3+} ions were calculated by the difference in initial and final concentrations. The effects of pH (2-9) and contact time (20–180 min)

were studied to achieve optimum performance of Fe^{3+} adsorption.

2.4 Calcium Adsorption Experiments

Batch calcium adsorption experiments were performed following the method of²⁵. Water with Ca^{2+} ion concentrations of 9.7, 19.4, 24.2, 36.1, and 48.0 mg/dm^3 were prepared by using CaCl_2 (Merck, Germany) dissolved in distilled water. The pH of the synthetic and tap waters was between 8.0 and 8.7. For Ca^{2+} adsorption experiments, filter (0.1 g) was added to 50 cm^3 of Ca^{2+} solution (9.7, 19.4, 24.2, 36.1, and 48.0 mg/dm^3) in a conical flask. The suspension was shaken continuously at 120 rpm and a temperature of 32 ± 2 °C. Following the adsorption, the aqueous phase was separated by centrifugation at 4000 rpm for 10 min and the final concentration of Ca^{2+} ion in the solution was determined by FAAS with air-acetylene and cathode on a Ca-hollow cathode lamp at 427.7 nm. The adsorbed amount of Ca^{2+} was calculated as well that of Fe^{3+} .

2.5 Removal Efficiency of Fe^{3+} and Ca^{2+} Ions

Final concentrations (C_f) of Fe^{3+} or Ca^{2+} were measured for the calculation of Fe^{3+} and Ca^{2+} removal percentages as shown in the eq. (1)²⁶:

$$\text{Removal\%} = ((C_o - C_f)/C_o) \times 100 \quad (1)$$

where C_o is the initial Fe^{3+} or Ca^{2+} ion concentration (mg/dm^3); C_f is the final Fe^{3+} or Ca^{2+} ion concentration (mg/dm^3). The adsorption capacity (Q_t , mg/g) at any time was calculated using a mass balance equation as shown in the eq. (2)²⁶:

$$Q_t = (C_o - C_f) \times (V/W) \quad (2)$$

Where V is the volume of the solution (dm^3); W is the mass of dry modified pineapple carbon fiber filter used (g).

2.6 Adsorption Isotherms

All of the experimental adsorption data were fitted with both the Langmuir equation and the Freundlich equation.

The rearranged Langmuir equation is:

$$Q_e = (Q_{max} K_L C_e) / (1 + K_L C_e) \quad (3)$$

where Q_e (mg/g) is the amount of solution adsorbed per unit mass of adsorbent, C_e (mg/dm³) is the Fe³⁺ or Ca²⁺ equilibrium concentration, Q_{max} (mg/g) is the maximum Fe³⁺ or Ca²⁺ amount that forms a complete monolayer on the surface, and K_L (dm³/mg) is the Langmuir constant related to adsorption heat. The linear form of this equation after rearrangement is:

$$C_e/Q_e = 1/(Q_{max} K_L) + C_e/Q_{max} \quad (4)$$

The constants Q_{max} and K_L can be determined from the slope and intercept of plotting C_e/Q_e against C_e ²⁷, respectively.

Freundlich model is used to estimate the adsorption intensity of KMnO₄ modified pineapple leaf carbon fiber filter towards the Fe³⁺ or Ca²⁺ ions and the equations is as follows:

$$Q_e = K_F C_e^{(1/n)} \quad (5)$$

This equation is conveniently used in linear form as²⁷:

$$\log Q_e = \log K_F + 1/n \log C_e \quad (6)$$

where Q_e and C_e have the same definitions as those in the Langmuir equation cited above. K_F and n are Freundlich constants related to adsorption capacity and heterogeneity factor, respectively. The constants K_F and n can be determined from the intercept and slope of plotting $\log Q_e$ against $\log C_e$, respectively.

3. Results and Discussion

3.1 The Physical Properties and Mass Yield

From Figure 1, it can be seen that the surfaces of the sintered filters have a brick color (Figure 1(b), Figure 1(c), and Figure 1(d)) as compared to the starting filters, which have a black color (Figure 1(a)). It shows that the some carbon fibers of the filters have undergone thermal

degradation. It is also apparent that more degradation is observed as the sintering temperature is increased from 500°C to 700°C. However, the inside texture of the sintered filters is still partially black. This shows that the carbon fibers are most degraded on the filter surface, which could be explained by clay mineral layers acting as insulators and a mass transport barrier to the volatile products generated during thermal decomposition²⁸. The brick color of the sintered filter is due to the presence of iron oxide²⁸ during sintering, which originates from the Fe content of the starting clay minerals. The black color intensities of the sintered filters decrease with increasing sintering temperature from 500 °C to 700 °C (Figure 1(b), Figure 1(c), Figure 1(d)). It was observed that the filter sintered at 700 °C is quite broken, which means that the filter fabricated with sintering at 700 °C possesses low hardness. As can be seen in Table 2, the drying shrinkages of the filters are increasing as the content of the fiber carbon is decreased and the zeolite content increased. Likewise, the firing shrinkage, increases with decreasing carbon fiber content and increasing sintering temperature. As a result, the total shrinkages are increased with increasing sintering temperature and decreasing carbon fiber content of the starting filters. On the other hand, the mass yields of the filters after sintering are decreased with increasing sintering temperature and increasing carbon fiber content of starting filters. The mass loss is related to the loss of surface-absorbed water (free water), interlayer water, dehydroxylation of the clay sheets²⁹, and carbon²⁸. The densities of the sintered filters increase with increasing sintering temperature and decreasing carbon fiber content. This trend is correlated with the increase of total of shrinkage. This result is due to the release of volatile matter from all starting materials at high sintering temperatures³⁰. Another reason is the presence of the clay minerals, which are thermally stable inorganic materials with high density³¹. The hardness of the sintered filters also decreased with increasing sintering temperature and increasing carbon fiber content. This is attributed to the amount of carbon fiber of sintered filter, which decreases with increasing sintering temperature and decreasing carbon fiber content of starting filter mixtures. The remaining carbon fiber in the sintered filters ensures interfacial interaction between carbon fiber and clay matrix by interlocking³² within the sintered filter. However at the sintering temperature of 700 °C, the hardness of sintered filter is lower than the limit set by the Thai Industrial Standards Institute (7.1380 kg/cm²)³³.

Table 2. Percent of drying shrinkage, firing shrinkage, total shrinkage, and mass yield of mixture samples of filters with sintering at 500-700°C

No. Samples	Temperature °C	% drying shrinkage	% firing shrinkage	% total of shrinkage	Mass yield (wt%)	Density (g/cm^3)	Hardness kg/cm^2
1	500	2.91	3.21	6.12	76.27	0.27	14.25
1	600	2.87	3.92	6.79	62.80	0.35	10.27
1	700	2.95	4.03	6.98	58.34	0.41	7.04
2	500	3.25	4.01	7.26	79.67	0.32	13.85
2	600	3.32	4.72	8.04	67.53	0.46	11.02
2	700	3.21	5.34	8.55	63.92	0.52	7.01
3	500	4.00	4.17	8.17	80.35	0.42	12.54
3	600	4.12	4.84	8.96	72.95	0.56	9.43
3	700	4.03	5.52	9.55	68.75	0.68	6.97

3.2 Elemental Composition

Table 3 shows the EDS analysis results for selected samples. It shows that the carbon content of carbonized pineapple leaf fiber after carbonization at 500°C is increased in comparison to the starting pineapple leaf fiber. This is because the volatile matter from the pineapple leaf fiber undergoes thermal degradation³⁰. The carbon content decreased after activation with H_3PO_4 , and modification with KMnO_4 , and further more decreased with mixing in of clay minerals. This is attributed to the thermal degradation and oxidation of carbon content²⁸ leading to a higher content of clay minerals. After the H_3PO_4 activation, the P content of the pineapple leaf carbon fiber is significantly increased. This indicates that the P is accumulated on the carbon fiber. Furthermore, after KMnO_4 modification, contents of K and Mn elements of the modified activated carbon fiber are also increased. This shows that K and Mn are also accumulated on the carbon fiber. It was seen that the P element remained on the carbon fiber after KMnO_4 modification. It can be concluded that the P atom formed a chemical bond to the carbon fiber, which is manifested by the presence of functional groups on the surface such as $\text{P}=\text{O}$, $\text{P}-\text{O}-\text{C}$ linkage, $\text{P}=\text{OOH}$, and $\text{P}-\text{O}-\text{P}^{34}$. In the case of the sintered filters, it was found that the content of Si and Al elements has increased as these elements originate from the clay minerals. This resulted in a further reduction of the C content. However, the K, Mn, and P elements remain in the filter. Analysis of the surface of the carbon fibers of the filter with EDS confirmed that the K, Mn, and P atoms are still present on the carbon fiber of the filter after sintering. Many of the samples contain a high amount of oxygen. This finding points to the presence

oxygen containing functional surface groups such as carboxyl, carbonyl, phenol, lactone, and other³⁵, being present in all of the samples. These results are linked to the physical properties and mass yield (Table 2).

3.3 FTIR Analysis

Figure 2 shows the FTIR transmissions for activated carbon fiber after H_3PO_4 activation, KMnO_4 modified pineapple carbon fiber, and KMnO_4 modified activated carbon fiber filter. It compares the pineapple leaf carbon fiber after H_3PO_4 activation using a 1:1 (volume: weight) ratio of 85% H_3PO_4 and pineapple leaf carbon fiber, the 5wt% KMnO_4 modified activated carbon fiber, and the 5wt% KMnO_4 modified fiber carbon filter after mixing with clay, zeolite, and bentonite. For activated carbon fiber (Figure 2(a)), the spectrum shows the peaks of OH vibrations (broad band between 2550-3600 cm^{-1}), P-H vibrations (at 2350 cm^{-1}), C=O group vibrations (at 1625 cm^{-1}), PO_4^{3-} vibrations (at 1160, 1000, 875, and 490 cm^{-1})³⁶, and C-O group vibrations (which overlap with phosphate bands at 1160 cm^{-1})¹⁹. After KMnO_4 modification (Figure 2(b)), the modified pineapple carbon fiber also shows peaks of O-H stretching (at 3400-2500 cm^{-1}), O-H bending (at 1225 cm^{-1}), and C-O stretching (at 1100 cm^{-1})³⁷, which as appeared as a result of KMnO_4 activation. Vibrations belonging to the PO_4^{3-} group were also found at about 1000 cm^{-1} . The presence of MnO_2 in KMnO_4 modified activated carbon fibers was confirmed by peaks in range 400 to 800 cm^{-1} at wave numbers such as 650 cm^{-1} , 500 cm^{-1} , and 450 cm^{-1} ³⁸⁻⁴⁰. In the case of the filters (Figure 2(c)), the IR spectrum shows the peaks of SiO-H groups (at 3750 cm^{-1}), tetrahedral Al ions (at about 1000 cm^{-1}), and Al-O or Si-O symmetric stretching

3.5 Textural Characteristics.

Table 4 shows BET surface area, pore volume, and average pore size of a select group of samples. It can be seen that activated carbon fiber, after H_3PO_4 activation at 500°C , has higher surface area and pore volume than carbon fiber carbonized at 500°C . However, the trend of the average pore size is reverse. This is due to the presence of H_3PO_4 in the impregnated carbon fibers during such high temperature conditions, which cause structural expansion in the activated carbon fiber that is being activated. This results in the surface area and the pore volume being increased. New micropores are created below 500°C , which is consistent with a report⁴⁷. After modified of the activated carbon fibers with KMnO_4 the surface area and pore volume of the modified activated carbon fibers are lowered. On the other hand average pore size of the material is increased. It seems that KMnO_4 modification

leads to the formation of bigger mesopores, which leads to a lower surface area and pore volume⁴⁸. Finally, surface area and average pore size of the filters prepared using sintering at 500°C are even lower. However, the pore volume of these materials is relatively higher. This is attributed to the coalescence behavior⁴⁹ between clay minerals and modified activated carbon fibers in the sintered filters, which results in lowering of surface area and average pore size of the filter. In contrast, the pore volume of sintered filters is increased. This is attributed to the degradation of volatile matter contained in clay minerals and carbon^{28–29} of the starting filter. Another reason is the porosity of zeolite with high content of the glassy phase after sintering, which exhibits high porosity⁵⁰.

3.6 SEM-EDS Analysis

Figure 4 shows the SEM morphology of a final filter. It can

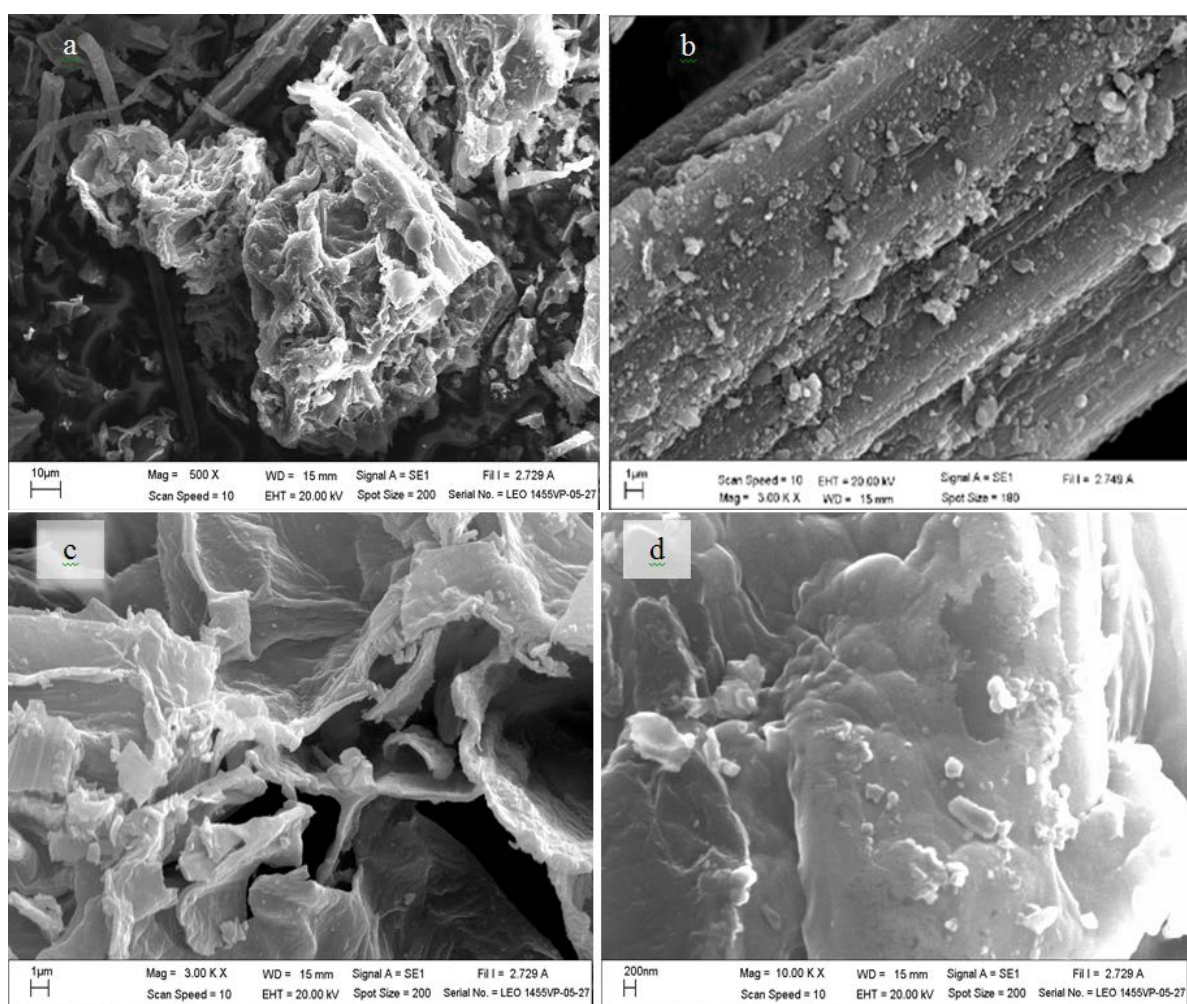


Figure 4. SEM morphology of filter after sintering at 500°C , (a) overview at 500x, (b) view of carbon fiber only (c) surface texture at 3000x and (d) surface texture at 10000x.

Table 4. BET surface area, pore volume, and average pore size of the samples

Samples	BET surface area (m ² /g)	pore volume (cm ³ /g)	Average pore size (nm)
PCF at 500 °C	106.7863	0.067077	2.51258
PACF at 500 °C	534.3411	0.25933	1.9413
5KPACF	211.9945	0.050387	4.2014
5KPACF Filter at 500 °C sintering	167.4968	0.08698	2.0772

be seen that the carbon fibers are distributed throughout the filter texture (overview in Figure 4(a)). It was shown that the carbon fibers exist in the filter after sintering at 500°C. It can be seen that small particles with different sizes are present on the surface of KMnO₄ modified activated carbon fiber. Based on the EDS analysis of this surface, the elemental composition of the surface of this carbon fiber is C, O, Mg, Al, Si, P, K, Mn, Ca, and Fe (Table 3). These elements originate from all of the raw materials e.g. Carbon fibers, H₃PO₄, KMnO₄, clay, zeolite, and bentonite. As focus view on the clay minerals with 3000x expansion (Figure 4(c)) shows a porous structure with wallplate wave character. When an expansion of the wallplate structure is made at magnification of 10000x (Figure 4(d)) wave surface with small particle and micropores can be observed.

3.7 Effect of Contact Time and pH on

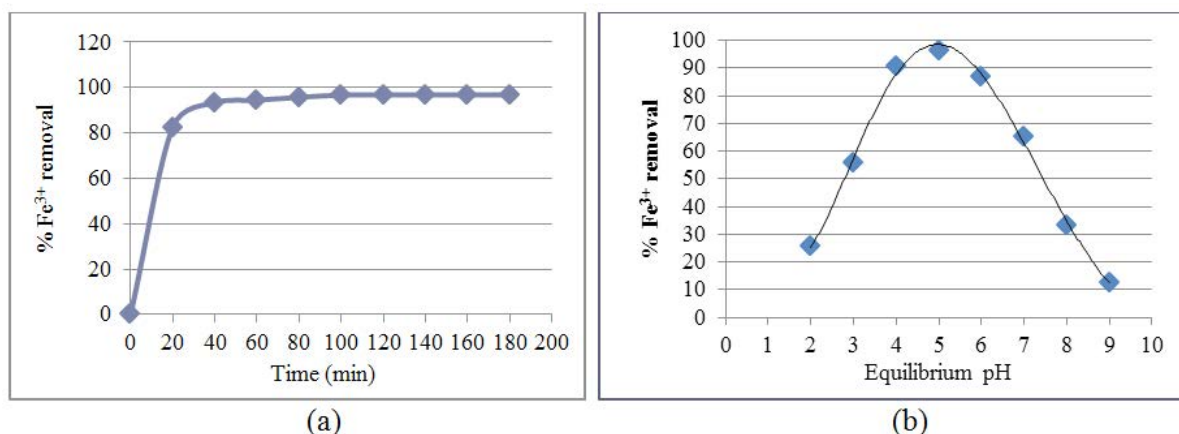
Adsorption of Fe³⁺ Ions

Figure 5(a) shows the effect of contact time of 5 mg/dm³ Fe³⁺ solution with filter at pH 5. It can be seen that the equilibrium for Fe³⁺ ion adsorption is achieved after about 60 min contact time with about 95% efficiency of removal. Figure 5(b) confirms that the maximum pH for Fe³⁺ ion adsorption by these filters is about 5, which is due

to low hydrogen ion competition from the solution. At pH >5, the Fe³⁺ adsorption becomes rapidly less efficient, which is due to the increased Fe³⁺ hydrolysis⁵¹. On the other hand, the Fe³⁺ adsorption at pH < 5 is also low. This could be explained by protonation of active sites of the filter at low, resulting in competition between H⁺ ions and Fe³⁺ ions for the binding sites²¹. Therefore pH 5.0 was selected for the further Fe³⁺ adsorption experiments.

3.8 Fe³⁺ Ions Adsorption Isotherm

Figure 6 shows Langmuir adsorption isotherm plot (Figure 6(a)) and Freundlich adsorption isotherm plot (Figure 6(b)) of Fe³⁺ adsorption for 5% KMnO₄ modified activated carbon fiber filter. It shows that the data of Fe³⁺ adsorption by the filter can be fitted with both the Langmuir isotherm and the Freundlich isotherm ($R^2 = 0.9999$ and 0.9978 , respectively). The Q_{max} and K_L values are 45.25 mg/g and 221.00 dm³/g, respectively. The theoretical maximum adsorption capacity for Fe³⁺ on KMnO₄ modified activated carbon filter is higher than that of nano-hydroxyapatite chitin/chitosan hybrid biocomposites (4.238-6.753 mg/g)¹⁹, carboxymethylated chitosan hydrogels (18.5 mg/g)¹⁸, and double template imprinted sorbent (36.90 ± 3.16 mg/g)²¹. It is also higher than for KMnO₄ modified carbon prepared

**Figure 5.** Effect of (a) contact time and (b) pH, on Fe³⁺ removal efficiency.

from waste of pineapple leaf fiber without clay minerals (25.25 mg/g)⁵². It was shown that the mineral clays have a significant effect on Fe^{3+} adsorption due to high density of functional groups and porous structure as showed in Figure 2 and Table 3. The dimensionless parameter (R_L) values of Fe^{3+} Langmuir adsorption isotherm (0.0004523-0.00151) of the filters indicate the adsorption to be favourable ($0 < R_L < 1$)⁵¹ under these conditions. This means that the Langmuir adsorption isotherm describes well the Fe^{3+} adsorption process by KMnO_4 modified activated pineapple carbon fiber filter, using the assumption that the Fe^{3+} ions are homogeneously distributed in a monolayer⁵³ over the KMnO_4 modified filter surface. In case of the Freundlich isotherm, the fitting of the data provided K_F and n with values of $44.6684 \text{ dm}^3 \text{ (1/n) mg}^{(1-1/n)}/\text{g}$ and 28.409, respectively. The high values of these two parameters reveal that the adsorption capacity and adsorption intensity of Fe^{3+} ions on the modified filter are high and a very strong adsorption is observed⁵³. It is noteworthy that the value of n is significantly greater than 1, which indicates very high heterogeneity²⁷ of the filter. It was seen that both adsorption isotherm models fit well the Fe^{3+} adsorption data of the filter. This is due to the fact that a low Fe^{3+} concentration (5 mg/dm^3) was used for this adsorption experiment. Thus, Fe^{3+} ions may adsorb in a monolayer on filter, which has heterogeneous surface as shown in SEM image (Figure 4).

3.9 Adsorption of Ca^{2+} Ions

Figure 7 shows the Ca^{2+} adsorption isotherm plots. It

can be seen that they are similar to the Fe^{3+} adsorption plots. Both the Langmuir isotherm and the Freundlich isotherm models could be fitted with Ca^{2+} adsorption data. But R^2 values for both these isotherms are lower than for the Fe^{3+} adsorption isotherms. This is because the Ca^{2+} concentration used in the experiments ($9.7\text{--}48.0 \text{ mg/dm}^3$) is quite higher than the Fe^{3+} concentration ($3\text{--}9 \text{ mg/dm}^3$) used for adsorption experiments. It was observed that the R^2 value for the Freundlich isotherm of the Ca^{2+} adsorption data is relatively higher than that of the Langmuir isotherm. It may be attributed to the Ca^{2+} adsorption on the filter taking place in a more complicated structure than just a monolayer. The other reason is attributed to the Ca^{2+} adsorption experiment, which follows the method of²⁵. In this experimental method, the total hardness of the solutions is maintained at a constant level using Ca^{2+} , Mg^{2+} , and NaHCO_3 . Therefore the Ca^{2+} adsorption experiments took place under competition from Mg^{2+} ions, which are assumed to have a higher adsorption rate than Ca^{2+} .⁵⁴ As a result, the five parameters obtained from the two isotherms for Ca^{2+} adsorption quite lower than for the Fe^{3+} adsorption isotherms. The values of Q_{max} , K_L , R_L , K_F , and n are $= 23.53 \text{ mg/g}$, $1.6410 \text{ dm}^3/\text{g}$, $0.01254\text{--}0.0591$, $12.5199 \text{ dm}^3 \text{ (1/n) mg}^{(1-1/n)}/\text{g}$, and 2.7465, respectively. This reveals that Ca^{2+} adsorption, according to the Langmuir isotherm, is still favourable under these conditions. However, adsorption capacity, adsorption intensity, and adsorption force for Ca^{2+} ions on the modified filter is lower than for Fe^{3+} adsorption. It may also be due to the competition between Ca^{2+} and Mg^{2+} ions. The Ca^{2+}

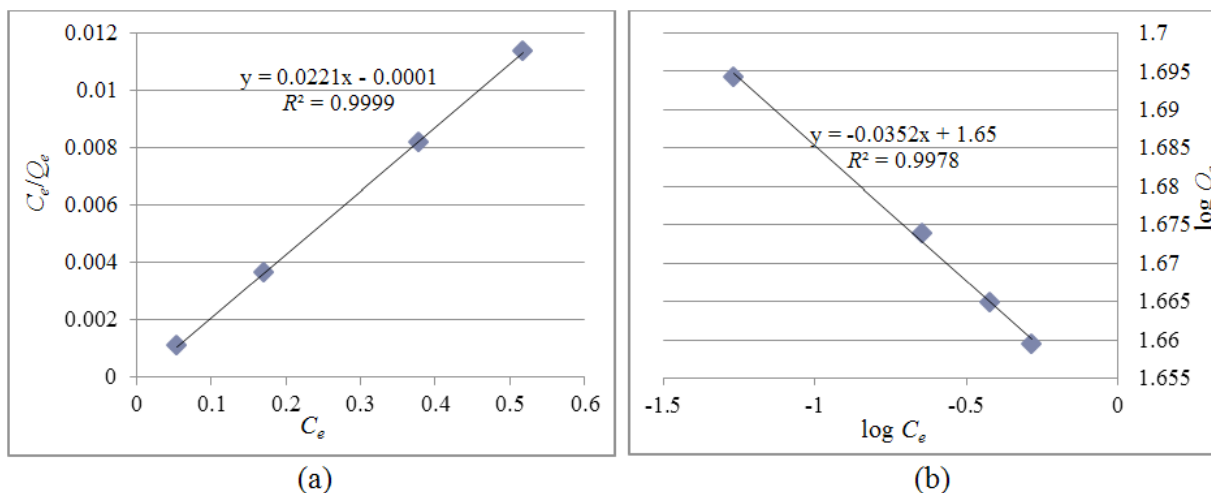


Figure 6. Fe^{3+} Langmuir adsorption isotherm plot (a) and Fe^{3+} Freundlich adsorption isotherm plot (b) for 5% KMnO_4 modified activated carbon fiber filter.

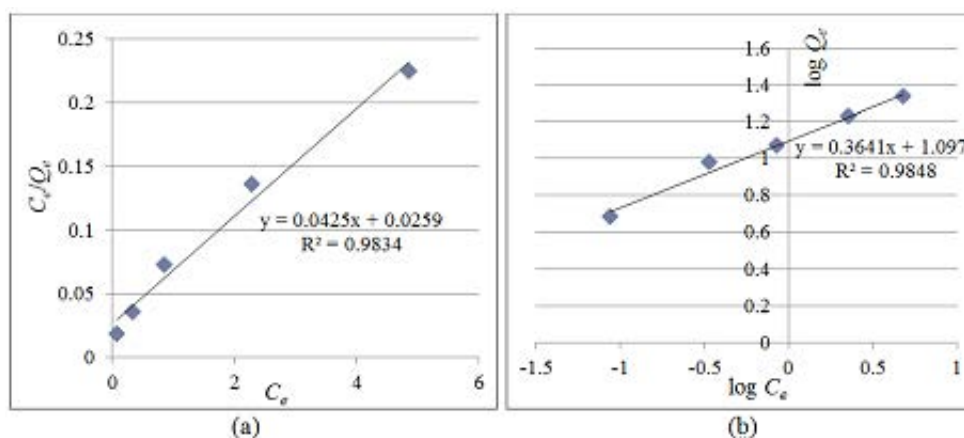


Figure 7. Langmuir isotherm plots (a), and Freundlich isotherm plot (b) for Ca^{2+} ion adsorption by 5% KMnO_4 modified pineapple activated carbon fiber filter.

adsorption on KMnO_4 modified activated carbon filter is also higher than on KMnO_4 modified carbon prepared from waste of pineapple leaf fiber without clay minerals (4.37–8.95 mg/g)⁵⁵.

4. Conclusion

Shrinkages (6.12–9.55%) and densities (0.27–0.68 g/cm³) of modified filters increased with increasing sintering temperature (500 °C to 700 °C) and decreasing carbon fiber content (60 wt% to 40 wt%). On the other hand, hardness (from 14.25 kg/cm² to 6.97 kg/cm²) and mass yields (from 80.00% to 58.34%) of modified filter exhibited a reverse trend. The values of these properties are within the requirements of the Thai Industrial Standards Institute, except for those prepared with sintering at 700 °C. The interfacial interactions between carbon fibers and clay matrix were improved by interlocking in the interior of the sintered filter. Many functional surface groups, oxide compounds, and clay minerals exist in filters such as MnO_2 , Si and Al oxides, P- and O-containing functional groups, montmorillonite, and kaolinite. These constituents have a positive effect on the adsorption properties for Fe^{3+} and Ca^{2+} by enabling ion exchange or complexation. The values of BET (167.50 m³/g), pore volume (0.08698 cm³/g) and average pore size (2.0772 nm) of sintered filters are quite lower than those of the starting materials due to occlusion of surface functional groups and composites on filter surface. Langmuir isotherm and Freundlich isotherm were fitted for both Fe^{3+} and Ca^{2+} adsorption with high R^2 values. However,

the parameter values from both Langmuir isotherm and Freundlich isotherm of Ca^{2+} adsorption are significantly lower than for Fe^{3+} adsorption. The theoretical maximum adsorption capacities of Fe^{3+} and Ca^{2+} for the modified filter are 45.25 and 23.53 mg/g, respectively, which are higher than for KMnO_4 modified carbon prepared from waste of pineapple leaf fiber without clay minerals. This emphasizes that the clay minerals have an effect on metal ion adsorption.

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