Application of Passivity to Adaptive Control Compensation Systems

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Abstract

In this paper the Model Reference Adaptive System (MRAS) is considered. The feedforward gain adjustment is done by using adaptive technique and feedforward gain compensation by passivity-based technique is presented. The adaptation of feedforward gain is considered by using MIT rule and the effect of variation of parameter values and adaptation gain on the response of the system is simulated. But to achieve more stable system, lyapunov stability theorem is used for parameter adjustment. It has been shown that the adjustment rule guarantees that error goes to zero. Finally input-output stability theorem is used to construct adjustment rules for the adaptive system. The passivity theorem is applied to construct adjustment laws. The compensating network is introduced so that the transfer function relating the error is Strictly Positive Real (SPR). The compensator is designed by using Kalman – Yakubovich (KY) Lemma. Simulation results are furnished after implementing the adaptive techniques. Algorithm for the design of compensator using KY Lemma is also presented.

Keywords: Feedforward Gain, KY Lemma, MIT Rule, Parameter Adjustment, Passivity, Strictly Positive Real

1. Introduction

The Model Reference Adaptive Control (MRAC) technique has been a popular approach to the control systems operating in the presence of parameter and environmental variations. The MRAC system was first designed by the performances index minimization method proposed by Whitaker of MIT Instrumentation laboratory and since then has been referred as the MIT rule. This rule has been very popular because of its simplicity in practical implementation. In this technique output rate of convergence depend upon the adaptation gain¹⁻³.

The other approach to adaptation is based on Lyapunov's second method. The adaptive rule is obtained by selecting the design equations to satisfy conditions derived from Lyapunov's second method⁴, so that the system stability is guaranteed for all inputs. The quadratic Lyapunov function was employed by Parks to redesign systems formerly designed by MIT rule. The main disadvantage of Lyapunov method is that the entire state vector must be available for measurement, which is not often possible^{4,5}.

The concept of positive realness plays a central role in stability theory in general and in many of the stability proofs of adaptive systems^{1,6}. The definition of Positive Real (PR) function of a complex variable *s* arises in circuit theory. Brune showed that the driving point impedance of a passive network is rational and positive real. If the network is dissipative, due to the presence of resistors, the driving point impedance is strictly positive real. In other words, a PR and SPR rational function can be realized as the driving point impedance of passive network. In this context KY lemma finds applications in adaptive control theory⁶.

The passivity theorem^{1,7} is invoking for the problem under consideration and it can be shown that the MRAS can be viewed as a feedback connection of two systems. By using passivity theorem it is possible to construct a stable

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adjustment law. For this a simple compensating network is introduced so that the transfer function relating the error is SPR. The proper compensator is found by using algorithm that based on KY Lemma⁷.

2. Adaptation by MIT Rule

2.1 MIT Rule

Consider a closed loop system in which a controller has one adjustable parameter θ . A model whose output is y_m specifies the desired closed loop response¹. Let *e* be the error between the output *y* of the closed loop system and the output y_m of the model. To adjust the parameters in such way that the loss function $J(\theta) = \frac{1}{2} e^2$ is minimized. To make *J*

small, it is possible to change the direction of the negative gradient of *J*, i.e.

$$\frac{d\theta}{dt} = -Y\frac{\partial J}{\partial \theta} = -Ye\frac{\partial e}{\partial \theta} \tag{1}$$

This is the well-known MIT rule. The partial derivative $\partial e/\partial \theta$, which is called the sensitivity derivative of the system and tells about the influence of error due to parameter variation.

2.2 Statement of the Problem

The problem under consideration is to adjust feedforward gain. In this problem it is assumed that the process is linear with the transfer function kG(s), where G(s) is known and k is unknown parameter². The design problem is to find a feedforward controller that gives a system with the transfer function $G_m(s) = k_0 G(s)$, where k_0 is given constant. With the feedforward controller $u = \theta u_c$. Where u is the control signal and u_c is the command signal and assuming parameter $\theta = k_0/k$.

The problem is described by following block diagram.

Now using the MIT rule to obtain a method for adjusting the parameter θ when k is not known. From Figure 1.

$$y = kG \left(\frac{d}{dt} \right) \theta Uc, \tag{2}$$

ym = ko G (d/dt) UcThe error is $e = y - ym = kG(d/dt) \theta Uc - koG(d/dt) Uc$ (3)



Figure 1. Block diagram of feedforward gain adaptation problem.

$$= kG \left(\frac{d}{dt} \right) \left(\theta - \theta \theta \right) Uc \tag{4}$$

Where d/dt is differential operator and $\theta^0 = k_0/k$

Partial derivative of Equation 3 with respect to θ is taken to obtain the sensitivity as –

$$\frac{\partial e}{\partial \theta} = kG(d/dt)u_c \tag{5}$$

but from equation (3), $G(d/dt)u_c =$ therefore Equation 5 becomes

$$\frac{\partial e}{\partial \theta} = \frac{k}{k_0} y_m \tag{6}$$

As per the MIT rule Equation 1 the adaptation law can be written as -

$$\frac{d\theta}{dt} = -Y'\frac{k}{k_0}y_m e = -Yy_m e \tag{7}$$

after integrting both sides of Equation 7,

$$\theta(t) = -Yy_m \int_{-\infty}^{t} e(s)ds \tag{8}$$

where $Y = Y' \frac{k}{k_0}$, Equation 8 gives the law for adjusting the parameter.

2.3 Simulation of the System

The adjustment mechanism of Figure 1 can be thought of as composed of three parts – a linear filter for computing the sensitivity derivative from inputs and outputs, a multiplier, and an integrator³.

Now by using MATLAB Simulink for simulation of the block diagram shown in Figure 1 and implementing

the feedforward gain adjustment law obtained by MIT rule Equation 8. For this purpose let us consider the transfer function

$$G(s) = \frac{s^2 + 4s + 3}{s^3 + 5s^2 + 6s + 1}$$
(9)

The simulation block diagram is shown in following Figure 2.

The input u_c is chosen as unit step or as sinusoidal of frequency 1 rad/sec selecting from source library⁴. The

parameters k, k_o are chosen as k = 1, and $k_o = 2$. The results of simulation are given by Figure 3 where y, y_m , θ , and eare shown for different y values, such as y = 0.5 and 0.75.

From Figure 3 it has been noted that, for both step and sinusoidal the response of the system depends on the adaptation gain. The convergence rate depends on the value of γ . For small value of γ convergence rate decreases and for high value of gamma convergence rate increases⁵. But there is no guarantee of the system stability in this adaptation technique.



Figure 2. Simulation block diagram for adjusting feedforward gain based on MIT rule.



Figure 3. Simulation of MRAS for adjusting a feedforward gain (a) Step Response for Adaptation gain = 0.5 and 0.75 (b) Sinusoidal Response for Adaptation gain = 0.5 and 0.75.

3. Adaptation by Lyapunov Theorem

The first step in the stability approach to adaptive system design is the choice of the adaptive law for adjusting the control parameters to assure stability. An alternative method for adaptation of MRAS based on Lyapunov's second method is suggested and here it is applied to the problem under consideration.

3.1 Lyapunov Theory

The problem of stability in previous method is considerably improved in this method. Now Lyapunov's stability theorem is used to construct algorithm for adjusting parameters in adaptive system⁶. For this let us consider a differential equation for error, $e = y - y_m$. This differential Equation contains the adjustable parameters. Then it is required to choose a suitable Lyapunov function and an adaptation mechanism so that the error goes to zero.

The error is given by Equation 4 and now using Lyapunov theorem^{1,4,7}, first consider the Equation of the system as –

$$e = Ae + k \left(\theta - \theta^{0}\right) u_{c} \tag{10}$$

writing state equations by considering the relation between the parameter θ and error *e* then,

$$\frac{dx}{dt} = Ax + b(\theta - \theta^0)u_c \ e = Cx \tag{11}$$

If the homogeneou s system x = Ax is asymptotic ally stable, there exist positive definite matrices P and Q such that $A^T P + PA = -Q$ (12) Now choosing the Lyapunov function as -

$$V = \frac{1}{2} (Y x^{T} P x + (\theta - \theta^{0})^{2})$$
(13)

$$\frac{dV}{dt} = \frac{Y}{2} - \frac{T}{dt}Px + x^{T}P\frac{dx}{dt} - (\theta - \theta^{0})\frac{d\theta}{dt}$$
(14)

by using equation 10, equation 13 becomes -

$$\frac{dV}{dt} = -\frac{Y}{2}x^{T}Qx + (\theta - \theta^{0})\frac{d\theta}{dt} + YUcB^{T}Px$$
(15)

therefore from equation (14) the parameter adjustment law is chosen to be -

$$\frac{d\theta}{dt} = -Yu_c B^T P x \tag{16}$$

From Equation 16, it is to be noted that, the derivative of Lyapunov function will be negative

as long as $x \neq 0$. The state vector x and the error e = Cx will go to zero as t goes to ∞ . But parameter error ($\theta - \theta^0$) will not necessarily go to zero. In this technique the restriction is that it requires that all state variables are known. A parameter adjustment law that uses output feedback can be obtained if Lyapunov function can be chosen such that $B^T P = C$, where *C* is the output matrix of the system⁷. Therefore,

 $B^T Px = Cx = e$, and the adjustment law becomes $\frac{d\theta}{dt} = -\gamma u_c e$ (17)

3.2 Simulation of the System

The control law obtained above Equation 17 is used to construct the adjustment mechanism of Figure 1 and modified by block diagram as shown in Figure 4, a



Figure 3. Simulation block diagram for adjusting feedforward gain based on lyapunov theory.

simulation diagram using MATLAB Simulink. Here again the input signal u_c is step and sinusoidal are applied to the system and simulation results are shown in Figure 5.

In this section it has been shown that it is possible to construct parameter adjustment rules based on Lyapunov's stability theory. The adjustment rules obtained in this way guarantee that the error goes to zero, but it cannot be asserted that the parameters converge to their correct values. Therefore some advanced technique like passivity is used to construct adjustment rules for the adaptive system⁸.

4. Adaptation by Passivity Theorem

The problem of feedforward gain compensation is the

main objective of this paper. In this section compensation obtained an adjustment rules based on passivity theorem. The same problem was treated in section 2 with Lyapunov's stability theory and obtained parameter adjustment law described by Equation 17. According to passivity theorem the adaptive system will be stable if the transfer function G(s) is SPR. This condition indicates that the result is related to passivity theory⁹.

4.1 Application of Passivity to Adaptive Control

The passivity theorem^{1,6,7} along with small gain theorem is used to derive stability results for the system under consideration Figure 1. Figure 6 shows a linear time invariant system described by G(s) and that corresponds to the plat together with a fixed controller, while the



Figure 5. Simulation of MRAS for adjusting a feedforward gain using lyapunov theory (a) Step response for adaptation gain = 0.5 and 0.75 (b) Sinusoidal response for adaptation gain = 0.5 and 0.75.



Figure 6. Block diagram for the system with adjustable feedforward gain when using the control law of Equation 17.

feedback system *H* corresponds to the mechanism generating the parameter error, θ and the corresponding control input $(\theta - \theta^0)u_c$. Thus passivity theorem^{1,7} is applied directly to such systems to prove L^2 – Stability if G(s) is strictly passive and *H* is passive.

The passivity theorem gives a convenient way to construct adjustable mechanism. For this simply introducing a compensating network so that the transfer function relating the error to $(\theta - \theta^0) u_c$ is SPR, and the compensator is designed by using algorithm given in Section 4.2. This mechanism is simulated as shown in Figure 7 and simulation results are shown in Figure 8 for sinusoidal input signals¹⁰⁻¹².

4.2 Algorithm based on KY Lemma for Designing Compensator

Step-1: By using KYP Lemma G(s) = B(s)/A(s) Finding polynomial C(s) such that C(s)/A(s) is SP Canonical realization of 1/A(s) is obtained by using *tf2ss* command of control system toolbox.

Step-2: Choosing a symmetric positive definite matrix *Q* and finding matrix P by using *lyap* command.

Step-3: The coefficients of a *C* polynomial such that C(s)/A(s) is SPR are then the first row of the P Matrix. i.e. C = P(1,:)

Therefore numerator polynomial of $G_c = C$ and denominator polynomial of G_c is polynomial of B(s).



Figure 7. A Stable Parameter Adjustment Law by Passivity and Ky Lemma.



Figure 8. Simulation of MRAS for a feedforward gain Compensation using KY Lemma (**a**) Step Response for Adaptation Gain = 0.5 and 0.75 (**b**) Sinusoidal Response for Adaptation Gain = 0.5 and 0.75.

5. Conclusion

The problem in which the system under consideration Figure 1, where adjustment mechanism replaced by MIT rule Equation 8 was performed well for the smaller adaptation gain but stability is disturbed for slightly increase in the γ value. Therefore the allowable range of the Gamma depends on the magnitude of the reference signal. Consequently it is not possible to give fixed limits which guarantee stability. Thus the MIT rule based adaptive systems are said to be closed loop unstable systems.

Adaptation based on Lyapunov's direct method guarantees the stability for all kinds of inputs and allows high gains in the adaptive loops i.e. adaptation gain, γ . From Figure 5 it has been seen that the stability of the system is asymptotic for the chosen *k*, k_o and γ values.

Adaptation mechanism due to passivity theorem along with small gain theorem and the design of compensator by using KY lemma is described in Figure 7. As per this arrangement it has been shown in Figure 8 that error e(s)goes to zero as *t* goes to infinity. MRAS of Figure 8 is stable for all values of $\gamma > 0$ when SPR condition is satisfied. This results in faster adaptation.

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